# Triclinic Cell Parameters from One Crystal Setting 

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#### Abstract

A general approach to determining triclinic cell parameters from one single-crystal setting is described, which has advantages over the method of angular lag. The procedure has been developed graphically, using a few chosen reflexions, but is also programmed for least-square computation, when a greater number of reflexions may be considered.


## Introduction

In examining compounds of particular chemical interest one is frequently presented with ill-formed crystals of low stability. In consequence, there are no faces to aid orientation, while time permits only a limited number of photographs to be taken before decomposition occurs. Buerger (1942) prescribes an angular lag procedure, but his treatment suffers from the practical defect that it requires two superposed Weissenberg exposures (zero and first layer), as well as depending upon measurements involving low index reflexions of type $h 00, h 01$ (if oscillating about the $c$ axis, for example) which may very well be unobservedly weak. The present method involves measurements between general $h k l$ reflexions and requires only that there be taken one oscillation photograph, one zero layer and one first layer equi-inclination Weissenberg photograph. The use of generalized Patterson and electron-density syntheses may then elucidate the essential features of the structure. Indeed, if the crystal is very unstable, an oscillation photograph plus a $100^{\circ}$ first layer Weissenberg photographs is sufficient to define cell parameters. Another advantage of the present procedure is that it works equally well whether or not the film holder is split into halves, as is customary in some forms of low temperature integrating cameras (e.g. Wiebenga \& Smits, 1950; Kreuger, 1955).

## Geometrical procedure

Let a crystal oscillate about the $c$ axis. $\zeta_{c}$ may be measured from an oscillation photograph, and $\xi_{a}, \xi_{b}$ and $\gamma^{*}$ are best measured from the zero layer Weissenberg photograph. Now consider the reciprocal lattice (Fig.1) where $O$ is the true origin and $D$ the origin of the $n$th layer projected down to $N$.
$N D$ is perpendicular to the $a^{*} b^{*}$ plane, and so corresponds to the direction of the $c$ axis.
$D P$ is drawn perpendicular to $O a^{*}$ and $Q N$ perpendicular to $D P$. $Q N$ will be the direction of the $b$ axis.

Thus $b \hat{N} c=\alpha$; therefore $Q \hat{P} N=Q \hat{N} D=180^{\circ}-\alpha$ and $\tan Q \hat{P} N=\tan \left(180^{\circ}-\alpha\right)=-\tan \alpha=D P / P N=n \zeta_{c} / \delta_{b}$ where $\delta_{b}$ is the shift of the $n$th layer origin perpendicular to $O a^{*}$.

Now the angular distance, $\varphi_{1}$, between any two reflexions $h_{1} k_{1} l$ and $h_{2} k_{2} l$ passing through the sphere of reflexion is readily measured from an $n$-layer equiinclination photograph, e.g. $\lambda$ between $1 \overline{1} 1$ and $\overline{1} 21$ in Fig. 2. It will, in general, differ from the angle between $h_{1} k_{1} 0$ and $h_{2} k_{2} 0$ because of the layer origin displacement.

We may thus construct on the $n$th layer of the reciprocal lattice the locus of points (a circle) at which the chord, $P_{1} P_{2}$ (Fig.3), subtends the angle $\varphi_{1}$. When $\varphi_{1}$ $<90^{\circ}$ this is most accurately achieved by joining $P_{1} P_{2}$, making $P_{2} X$ perpendicular to $P_{1} P_{2}$ and $X \hat{P}_{1} P_{2}$ equal to $90-\varphi_{1}$. The bisector, $U$, of $P_{1} X$ is then the centre of the required circle. If $\varphi_{2}>90^{\circ}$ (say) then the angle $\frac{1}{2}\left(180^{\circ}-\varphi_{2}\right)$ is constructed at $P_{3}$ and $P_{4}$, and two sides of the resultant triangle are bisected to give the centre, $V$, of the circumscribing circle.

Repetition for another pair of reflexions, angle $\varphi_{2}^{\prime}$, results in intersecting circles, and discrimination between the two points of intersection may be made by reference to a third pair of reflexions, angle $\varphi_{3}^{\prime}$, to obtain the projection of the displaced origin, $N^{\prime}$.
$\delta_{b}$, perpendicular to $O a^{*}$, may then be measured and the direct angle $\alpha$ calculated. The best accuracy is obtained when the circles intersect close to right angles.

## Computational procedure

The solution of the precise analytical expression is difficult, and a quickly converging iterative method is used.

Let the $n$th layer origin shifts parallel to the $a^{*}$ and $b^{*}$ axes (Fig.4) be $n A$ and $n B$ ( $\delta_{b}$ then equals $n B \sin \gamma^{*}$, etc.).

We may compute $\left(P_{1} P_{2}\right)^{2}$ in two ways to equal

$$
\begin{align*}
&\left(h_{2}-h_{1}\right)^{2} a^{2}+\left(k_{2}-k_{1}\right)^{2} b^{2} \\
&+2\left(h_{2}-h_{1}\right)\left(k_{2}-k_{1}\right) a b \cos \gamma^{*} \tag{1}
\end{align*}
$$

or
where

$$
\begin{equation*}
\alpha_{1}^{2}+x_{2}^{2}-2 \mid \alpha_{1}^{2} \alpha_{2}^{2} \cdot \cos \varphi_{1} \tag{2}
\end{equation*}
$$

$$
\begin{aligned}
\alpha_{1}^{2}=\left(h_{1} a+n A\right)^{2}+\left(k_{1} b\right. & +n B)^{2} \\
& +2\left(h_{1} a+n A\right)\left(k_{1} b+n B\right) \cos \gamma^{*}
\end{aligned}
$$

and similarly for $\alpha_{2}$.

Equating and gathering terms leads to equations of the form

$$
A x+B y=C_{0},
$$

where

$$
\begin{aligned}
& C_{0}=\left(-h_{1} h_{2} a^{2}-k_{1} k_{2} b^{2}-h_{1} k_{2} a b \cos \gamma^{*}\right. \\
&\left.-h_{2} k_{1} a b \cos \gamma^{*}\right)+\cos \varphi_{1} \cdot \sqrt{\alpha_{1}^{2}} \overline{\alpha_{2}^{2}}-2 n^{2} A B \cos \gamma^{*} \\
& x=n\left\{\left(h_{1} a+h_{2} a+k_{1} b \cos \gamma^{*}+k_{2} b \cos \gamma^{*}\right)+n A\right\} \\
& y=n\left\{\left(h_{1} a \cos \gamma^{*}+h_{2} a \cos \gamma^{*}+k_{1} b+k_{2} b\right)+n B\right\} .
\end{aligned}
$$

There will be several such equations, depending on how many angular distances are measured. Commencing with rough values, $A_{0}, B_{0}$, for $A$ and $B$, we may calculate $C_{c}=A_{0} x+B_{0} y$ so that

$$
\Delta C=C_{0}-C_{c}=\left(\frac{\partial C}{\partial A}\right) \Delta A+\left(\frac{\partial C}{\partial B}\right) \Delta B
$$

whence

$$
\Delta A=\frac{\Sigma \Delta C \cdot x}{\Sigma x^{2}} ; \quad \text { etc. }
$$

The strategy is to choose solutions, $A_{0}$ and $B_{0}$, compute $C_{0}, x$ and $y$, and to derive improved $A$ and $B$ values by three minor rounds of refinement, so that $A_{1}=A_{0}+A_{1}$, etc. At this point $C_{0}, x$ and $y$ are recalculated (as they depend upon the magnitude of $A$ and $B$ ) and another three rounds of refinement are carried out. By such an iterative process $A$ and $B$ are improved until they are no longer subject to significant changes


Fig. 1. General view of reciprocal lattice.


Fig. 2. Upper half of first layer equi-inclination Weissenberg photograph.
between major rounds. At this point the resultant $A$ and $B$ values are output, together with the angles $\alpha$ and $\beta$. In addition, the final calculated input angles, $\varphi_{c}$, are printed out for comparison with the measured $\varphi$ values employed.

In the program, written in Extended Mercury Autocode for the University of London Atlas Computer, starting values for $A$ and $B$ have been written in as 0.001 and 0.001 . Provided that at least eight values of $\varphi$ are introduced, which have values in the range 70$110^{\circ}$ (so that $\cos \varphi$ is not too large) only about five rounds of major refinement are needed. With $\varphi$ values around $40^{\circ}$ some twenty rounds of refinement may be needful.

## Accuracy

The accuracy obtainable is exemplified by some data, summarized in Table 1, relating to copper(II) sulphate pentahydrate which was oscillated in turn about each


Fig. 3. $n$th layer of reciprocal lattice, showing constructions to obtain the projected origin, $N^{\prime}$.


Fig. 4. $n$th layer of reciprocal lattice, showing a typical triangle used in computing the projected origin, $N^{\prime}$.

Table 1. Data for $\mathrm{CuSO}_{4} .5 \mathrm{H}_{2} \mathrm{O}$
Experimental values obtained by angular lag about axis below

$$
\begin{gathered}
a \text { axis } \\
b \text { axis } \\
c \text { axis } \\
\text { Literature values }
\end{gathered}
$$

| $x_{g}$ | Graphical \& p |  | programmed angles ( ${ }^{( }$) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\alpha_{p}$ | $\beta_{g}$ | $\beta_{p}$ | $\gamma_{g}$ | $p$ |
| - | - | $107 \cdot 4$ | 108.1 | $76 \cdot 8$ | 77.9 |
| $97 \cdot 1$ | 97.7 |  |  | $77 \cdot 1$ | $76 \cdot 8$ |
| $97 \cdot 4$ | 97.5 | $107 \cdot 3$ | $107 \cdot 2$ |  |  |
| 97.6 |  | $107 \cdot 2$ |  | 77.6 |  |

principal axis after being set by the procedure of Brooker \& Nuffield (1966). More detailed information is given for one axis in Table 2. In general the graphical

Table 2. Comparison of inter-reflexion angles, $\varphi_{m}$, measured with a ruler and those, $\varphi_{c}$, calculated from the final cell parameters deduced by programmed angular lag
Values marked * were used for graphical evaluation

| $h$ | $k$ | $l$ | $h$ | $k$ | $l$ | $\varphi_{m}$ | $\varphi_{c}$ |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 0 | 3 | 1 | 1 | 0 | 1 | $85 \cdot 5^{\circ}$ | $85 \cdot 4^{\circ}$ |
| 0 | 3 | 1 | 1 | -1 | 1 | $108 \cdot 0$ | $107 \cdot 7$ |
| 0 | 3 | 1 | 0 | 0 | 1 | $67 \cdot 0$ | $66 \cdot 7$ |
| 0 | 2 | 1 | 1 | 0 | 1 | $81 \cdot 0$ | $81 \cdot 0$ |
| 0 | 2 | 1 | 1 | -1 | 1 | $103 \cdot 0$ | $103 \cdot 2$ |
| $* 0$ | 1 | 1 | 1 | 0 | 1 | $69 \cdot 6$ | $69 \cdot 6$ |
| $* 0$ | 1 | 1 | 1 | -1 | 1 | $92 \cdot 0$ | $91 \cdot 9$ |
| 1 | 2 | 1 | 0 | -1 | 1 | $95 \cdot 5$ | $95 \cdot 5$ |
| 1 | 2 | 1 | 0 | -2 | 1 | $111 \cdot 0$ | $111 \cdot 2$ |
| $* 1$ | 1 | 1 | 0 | -1 | 1 | $76 \cdot 6$ | $76 \cdot 7$ |
| 1 | 1 | 1 | 0 | -2 | 1 | $92 \cdot 0$ | $92 \cdot 4$ |
| $* 0$ | 0 | 1 | 0 | -1 | 1 | $71 \cdot 5$ | $71 \cdot 5$ |
| 0 | 0 | 1 | 0 | -2 | 1 | $87 \cdot 5$ | $87 \cdot 3$ |
| -1 | -3 | 1 | -1 | 0 | 1 | $85 \cdot 0$ | $84 \cdot 5$ |
| -1 | -2 | 1 | -1 | 0 | 1 | $72 \cdot 0$ | $71 \cdot 5$ |
| -1 | -2 | 1 | -1 | 1 | 1 | $100 \cdot 6$ | $100 \cdot 4$ |
| $*-1$ | -1 | 1 | -1 | 1 | 1 | $73 \cdot 0$ | $72 \cdot 5$ |
| -1 | -1 | 1 | -1 | 2 | 1 | $86 \cdot 1$ | $86 \cdot 0$ |
| -2 | -2 | 1 | -1 | 1 | 1 | $71 \cdot 0$ | $70 \cdot 9$ |
| -2 | -2 | 1 | -1 | 2 | 1 | $84 \cdot 2$ | $84 \cdot 4$ |
| -1 | 0 | 1 | 0 | 2 | 1 | $83 \cdot 8$ | $83 \cdot 5$ |
| -1 | 0 | 1 | 0 | 3 | 1 | $79 \cdot 5$ | $79 \cdot 0$ |
| -2 | -1 | 1 | 0 | 3 | 1 | $103 \cdot 0$ | $103 \cdot 2$ |
| -2 | -1 | 1 | 0 | 2 | 1 | $107 \cdot 2$ | $107 \cdot 6$ |

method, provided some half-dozen values of $\varphi$ are taken and the various close intersections are finally averaged, is accurate to about $1^{\circ}$. With the least-square computational procedure, a rather better accuracy is obtainable, particularly if $\varphi$ angles are measured with a travelling microscope. The resultant cell angles are sensitive to errors in crystal setting.

The resulting $\alpha, \beta, \gamma^{*}$ values are used to calculate direct cell angles, and hence to obtain direct cell dimensions from $\xi_{a}$ and $\xi_{b}$. At this stage a Delaunay reduction (Delaunay, 1933, Patterson \& Love 1957,) may be applied to obtain the conventional triclinic cell, and to ensure that the crystal truly lacks elements of symmetry.

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